Phys. Med. Biol. 52 (2007) 7333-7352

# An exact approach to direct aperture optimization in IMRT treatment planning<sup>\*</sup>

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Received 22 July 2007, in final form 28 September 2007 Published 5 December 2007 Online at stacks.iop.org/PMB/52/7333

#### Abstract

We consider the problem of intensity-modulated radiation therapy (IMRT) treatment planning using direct aperture optimization. While this problem has been relatively well studied in recent years, most approaches employ a heuristic approach to the generation of apertures. In contrast, we use an exact approach that explicitly formulates the fluence map optimization (FMO) problem as a convex optimization problem in terms of all multileaf collimator (MLC) deliverable apertures and their associated intensities. However, the number of deliverable apertures, and therefore the number of decision variables and constraints in the new problem formulation, is typically enormous. To overcome this, we use an iterative approach that employs a subproblem whose optimal solution either provides a suitable aperture to add to a given pool of allowable apertures or concludes that the current solution is optimal. We are able to handle standard consecutiveness, interdigitation and connectedness constraints that may be imposed by the particular MLC system used, as well as jaws-only delivery. Our approach has the additional advantage that it can explicitly account for transmission of dose through the part of an aperture that is blocked by the MLC system, yielding a more precise assessment of the treatment plan than what is possible using a traditional beamlet-based FMO problem. Finally, we develop and test two stopping rules that can be used to identify treatment plans of high clinical quality that are deliverable very efficiently. Tests on clinical head-and-neck cancer cases showed the efficacy of our approach, yielding treatment plans comparable in quality to plans obtained by the traditional method with a reduction of more than 75% in the number of apertures and a reduction of more than 50% in beam-on time, with only a

\* This work was supported by the National Science Foundation under grant no. DMI-0457394.

0031-9155/07/247333+20\$30.00 © 2007 IOP Publishing Ltd Printed in the UK

<sup>&</sup>lt;sup>3</sup> This author owns stock in and is Chief Science Officer of ViewRay Incorporated and as such may benefit financially as a result of the outcomes of work or research reported in this manuscript.

modest increase in computational effort. The results also show that delivery efficiency is very insensitive to the addition of traditional MLC constraints; however, jaws-only treatment requires about a doubling in beam-on time and number of apertures used. Finally, we showed the importance of accounting for transmission effects when assessing or, preferably, optimizing treatment plan quality.

(Some figures in this article are in colour only in the electronic version)

#### 1. Introduction

Traditionally, intensity-modulated radiation therapy (IMRT) treatment plans are developed using a two-stage process. In particular, each beam is typically modeled as a collection of hundreds of small beamlets or bixels, and the intensities of each of these bixels are assumed to be controllable on an individual basis. The problem of finding an optimal intensity profile or fluence map for each beam, called the (beamlet-based) fluence map optimization (FMO) problem, must then be followed by a leaf-sequencing stage in which the fluence maps are decomposed into a manageable number of apertures that are deliverable using a multileaf collimator (MLC) system. The objective of this second stage problem is to accurately reproduce the ideal fluence map while limiting the total treatment time. More formally, in this second stage it is desirable to limit both the total time that radiation is delivered, i.e., the total beam-on time, and the total number of apertures used. Both the beamlet-based FMO problem and the leaf-sequencing problem are well studied in the literature. For modeling and solution approaches to the FMO problem we refer to the review paper by Shepard et al (1999). More recently, Lee et al (2000, 2003) studied mixed-integer programming approaches, Romeijn et al (2003, 2006) proposed new convex programming models, and Hamacher and Küfer (2002) and Küfer et al (2003) considered a multi-criteria approach to the problem. The problem of leaf sequencing while minimizing the total beam-on time is very efficiently solvable in general. We refer in particular to Ahuja and Hamacher (2005), Bortfeld et al (1994), Kamath et al (2003) and Siochi (1999); in addition, Baatar et al (2005), Boland et al (2004), Kamath et al (2004a-2004d), Lenzen (2000), Siochi (1999) and Dai and Hu (1999) studied the problem under additional MLC hardware constraints, while Kalinowski (2005b) studied the benefits of allowing rotation of the MLC head. The problem of decomposing a fluence map into the minimum number of apertures has been shown to be strongly NP-hard (see, Baatar et al (2005)), motivating the development of a large number of heuristics for solving this problem. Notable examples are the heuristics proposed by Baatar et al) (who also identified some polynomially solvable special cases), Dai and Zhu (2001), Que (1999), Siochi (1999) and Xia and Verhey (1998). In addition, Engel (2005), Kalinowski (2005) and Lim and Choi (2006) developed heuristics to minimize the number of apertures while constraining the total beam-on time to be minimal. Langer et al (2001) developed a mixed-integer programming formulation of the problem, while Kalinowski (2004) proposed an exact dynamic programming approach. Finally, Taşkın et al (2007) proposed a new exact optimization approach to the problem of minimizing the total treatment time.

A major drawback in the decoupling of the treatment-planning problem into a beamletbased FMO problem and a MLC leaf-sequencing problem is that there is a potential loss in the treatment quality. This has led to the development of approaches that integrate the beamletbased FMO and leaf-sequencing problems into a single optimization model, which are usually referred to as direct aperture optimization approaches to FMO. In this approach, we explicitly solve for a set of apertures and the corresponding intensities in a single aperture-based FMO problem. For examples of integrated approaches to fluence map optimization, sometimes also called aperture modulation or aperture-based fluence map optimization, we refer to Preciado-Walters *et al* (2004), Shepard *et al* (2002), Siebers *et al* (2002), Bednarz *et al* (2002) and Romeijn *et al* (2005). The way the dose distribution received by the patient is modeled in a beamlet-based FMO model is necessarily an approximation since this distribution depends not only on the intensity profile but also on the actual apertures used to deliver this profile. The current literature on aperture modulation has, however, not yet exploited the ability of aperture modulation to take into account such effects. In particular, while the leaves in the MLC system do block *most* of the radiation beam, there is some small but not insignificant amount of dose (on the order of 1.5-2%, see Arnfield *et al* (2000)) that is transmitted through the leaves in the MLC system. Finally, while several aperture-based FMO approaches attempt to limit the total treatment time by limiting the number of apertures used, these models do not explicitly incorporate the total beam-on time as a measure of treatment plan efficiency.

In this paper, we extend the approach developed by Romeijn *et al* (2005) by (i) allowing for the incorporation of more general treatment plan evaluation criteria, and (ii) accounting for transmission effects. In addition, we extend the method to MLC systems that can only deliver apertures that are rectangular in shape. Our goals in this paper are to

- evaluate the ability of our approach to efficiently find high-quality treatment plans with a limited number of apertures and beam-on time;
- evaluate the effect of MLC deliverability constraints on the required number of apertures and beam-on time;
- evaluate the importance of explicitly incorporating transmission effects.

#### 2. Direct aperture optimization

With most forms of external-beam radiation therapy, a patient is irradiated from several different directions, which we assume are chosen based on experience by a physician or clinician. We will denote the set of beam directions by *B*. Each beam  $b \in B$  is discretized into a matrix of bixels, indicated by the set  $N_b$ . For convenience we let  $N \equiv \bigcup_{b \in B} N_b$  denote the set of all bixels. We will denote the set of apertures that can be delivered by a MLC system from beam direction  $b \in B$  by  $K_b$  and the set of all deliverable apertures by  $K \equiv \bigcup_{b \in B} K_b$ . For convenience, we let  $b_k$  denote the beam that contains aperture k, i.e.,  $k \in K_{b_k}$  for all  $k \in K$ . Clearly, each aperture can then be viewed as a subset of bixels in a beam, so we will denote a particular aperture  $k \in K_b$  by the set of beamlets  $A_k \subseteq N_b$ . With each aperture  $k \in K$  we associate a decision variable  $y_k$  that indicates the intensity of that aperture.

The dose distribution in a patient is evaluated on a discretization of the three-dimensional geometry of the patient, obtained via a CT scan, into a number of voxels. We denote the set of all voxels by V, and associate a decision variable  $z_j$  with each voxel  $j \in V$  that indicates the dose received by that voxel. The vector of voxel doses can be expressed as a linear function of the intensities of the apertures through the so-called *dose deposition coefficients*  $\mathcal{D}_{kj}$ , the dose received by voxel  $j \in V$  from aperture  $k \in K$  at unit intensity.

Finally, we assume that a collection, say L, of *treatment plan evaluation criteria* has been identified that measure clinical treatment plan quality and are expressed as functions of the dose distribution:  $G_{\ell} : \mathbb{R}^{V} \to \mathbb{R}$  for  $\ell \in L$ . Each of these criteria is usually, but not necessarily, a function of the dose distribution in a particular structure only. Without loss of generality we assume that the criteria are expressed in such a way that smaller values are preferred to larger values. Finally, we assume that all criteria are convex. This is justified by the fact that most criteria proposed in the literature to date are indeed convex or can be replaced by a convex criterion that has the property that the Pareto-efficient frontier associated with all criteria is unchanged (see, Romeijn *et al* (2004)). Examples of such criteria are tumor control probability (TCP), normal tissue complication probability (NTCP), equivalent uniform dose (EUD), conditional value at risk (CVaR), voxel-based penalty functions, etc (see, e.g., Niemierko (1997, 1999), Lu and Chin (1993), Kutcher and Burman (1989), Rockafellar and Uryasev (2000) and Tsien *et al* (2003)).

Our aperture-based FMO model can now be formulated as follows:

minimize 
$$\sum_{\ell \in L} \gamma_\ell G_\ell(z)$$

subject to

(A) 
$$z_j = \sum_{k \in K} \mathcal{D}_{kj} y_k$$
 for all  $j \in V$  (1)

$$y_k \ge 0 \qquad \text{for all} \quad k \in K.$$
 (2)

Here  $z \in \mathbb{R}^{|V|}$  and  $y \in \mathbb{R}^{|K|}$  are the vectors containing the voxel doses and aperture intensities, respectively. Moreover, the coefficients  $\gamma_{\ell}$  ( $\ell \in L$ ) are nonnegative weights associated with the clinical treatment plan evaluation criteria. Many other aperture-based FMO models that have been proposed in the literature are heuristics that are based on deterministic or stochastic search, such as simulated annealing, for which it often cannot be guaranteed that all deliverable apertures are (explicitly or implicitly) considered. In contrast, our approach explicitly incorporates all deliverable apertures and corresponding intensities.

Traditional beamlet-based FMO models as well as all aperture-based FMO models to date have assumed that the dose deposition coefficients can be written as

$$\mathcal{D}_{kj} = \sum_{i \in A_k} D_{ij},\tag{3}$$

where  $D_{ij}$  is the dose received by voxel *j* from bixel *i* at unit intensity. However, this definition ignores any transmission and scatter effects that are due to the shape of the apertures used. Both of these effects cannot be modeled in a beamlet-based FMO model. In this paper, we will explicitly incorporate the transmission effect. In particular, the expression for the dose deposition coefficients given in (3) assumes that any bixel that is blocked in an aperture does not transmit any radiation. If we denote the fraction of the dose that is transmitted by  $\epsilon \in [0, 1]$ , we obtain the following expression for the dose deposition coefficients:

$$\mathcal{D}_{kj} = \sum_{i \in A_k} D_{ij} + \epsilon \sum_{i \in N_{b_k} \setminus A_k} D_{ij}$$
  
=  $(1 - \epsilon) \sum_{i \in A_k} D_{ij} + \epsilon \sum_{i \in N_{b_k}} D_{ij}$   
=  $(1 - \epsilon) \sum_{i \in A_k} D_{ij} + \epsilon \bar{D}_{b_kj},$ 

where  $\bar{D}_{bj} = \sum_{i \in N_b} D_{ij}$ . Clearly, the traditional expression (3) corresponds to the special case where  $\epsilon = 0$ .

#### 3. Column generation algorithm

#### 3.1. Introduction

It is clear that the number of allowable apertures (i.e., the cardinality of *K*) is typically enormous. For example, consider an MLC that allows all combinations of left and right leaf settings. Even with a coarse  $10 \times 10$  bixel grid and five beams, this would yield more than  $10^{18}$  deliverable apertures to consider. However, it is reasonable to expect that in the optimal solution to (A) only a relatively small number of apertures will actually have positive intensity. The challenge is therefore to identify a small but judiciously chosen set of apertures that yield a high-quality treatment plan. Since it does not seem possible to intuitively identify or characterize such a set of apertures for each individual patient, we use a formal column generation approach to solving the aperture-based FMO problem. This method starts by choosing a limited number of apertures, for example corresponding to a conformal plan, given by a set  $\hat{K} \subseteq K$ . It then solves a restricted version of (A) using *only* that set of apertures. Next, an optimization subproblem, called the *pricing problem*, is solved. This

- (i) identifies one or more promising apertures that will improve the current solution when added to the collection of considered apertures; or
- (ii) concludes that no such apertures exist, and therefore the current solution is optimal.

In case (i), we add the identified apertures to  $\hat{K}$ , re-optimize the new aperture-based FMO problem, and repeat the procedure. Intuitively, the pricing problem identifies those apertures for which the improvement of the objective function per unit intensity is largest (and therefore show promise for significantly improving the treatment plan). The very nature of our approach thus allows us to study the effect of adding apertures on the quality of the treatment plan, thereby enabling a sound trade-off between the number of apertures and treatment plan quality.

#### 3.2. Derivation of the pricing problem

Let us denote the dual multipliers associated with constraints (1) and (2) by  $\pi_j$  ( $j \in V$ ) and  $\rho_k$  ( $k \in K$ ). The Karush–Kuhn–Tucker (KKT) optimality conditions (see, e.g., Bazaraa *et al* (2006)) for (A), which are necessary and sufficient for optimality because of the convexity of the objective function and the linearity of the constraints, can be written as follows:

$$\pi_{j} = \sum_{\ell \in L} \gamma_{\ell} \frac{\partial G_{\ell}(z)}{\partial z_{j}} \quad \text{for all} \quad j \in V$$

$$\rho_{k} = \sum_{j \in V} \mathcal{D}_{kj} \pi_{j} \quad \text{for all} \quad k \in K$$

$$z_{j} = \sum_{k \in K} \mathcal{D}_{kj} y_{k} \quad \text{for all} \quad j \in V$$

$$y_{k} \rho_{k} = 0 \quad \text{for all} \quad k \in K$$

$$y_{k}, \rho_{k} \ge 0 \quad \text{for all} \quad k \in K.$$

Any solution to this system can be characterized by  $y \ge 0$  only: this vector then determines, in turn,  $z, \pi$  and  $\rho$ . Let  $(\hat{y}; \hat{\pi}, \hat{\rho})$  be an optimal pair of primal and dual solutions to a subproblem in which only apertures in the set  $\hat{K} \subset K$  are considered, where we have set  $\hat{y}_k = 0$  for  $k \in K \setminus \hat{K}$ . We can then conclude that this solution is in fact optimal for (A) if and only if  $\hat{\rho}_k \ge 0$  for all  $k \in K$  (note that this inequality is satisfied for  $k \in \hat{K}$  by construction).

In other words, if and only if the optimal solution to the following so-called *pricing problem* is nonnegative:

minimize<sub>$$k \in K$$</sub>  $\sum_{j \in V} \mathcal{D}_{kj} \hat{\pi}_j$ .

Since each aperture contains beamlets in a single beam only, we may alternatively solve a pricing problem for each individual beam  $b \in B$ :

minimize<sub>$$k \in K_b$$</sub>  $\sum_{j \in V} \mathcal{D}_{kj} \hat{\pi}_j$ .

Now note that if  $k \in K_b$  we have

$$\sum_{j \in V} \mathcal{D}_{kj} \hat{\pi}_j = \sum_{j \in V} \left( (1 - \epsilon) \sum_{i \in A_k} D_{ij} + \epsilon \bar{D}_{bj} \right) \hat{\pi}_j$$
$$= (1 - \epsilon) \sum_{j \in V} \sum_{i \in A_k} D_{ij} \hat{\pi}_j + \epsilon \sum_{j \in V} \bar{D}_{bj} \hat{\pi}_j.$$

This then means that the current solution is optimal for (A) if and only if, for all  $b \in B$ , the optimal solution to the following optimization problem

$$\operatorname{minimize}_{k \in K_b} \sum_{i \in A_k} \left( \sum_{j \in V} D_{ij} \hat{\pi}_j \right)$$

exceeds the threshold value

$$-\frac{\epsilon}{1-\epsilon}\sum_{j\in V}\bar{D}_{bj}\hat{\pi}_j.$$
(4)

We can now justify the intuition behind the pricing problem and the column generation algorithm that was provided earlier: realizing that  $\sum_{j \in V} D_{ij} \hat{\pi}_j$  measures the per-unit change in the objective function value if the intensity of beamlet *i* is increased; it follows that the pricing problem for a given beam identifies the aperture with the property that the rate of improvement in the objective function value, as the intensity of the aperture is increased, is *largest* among all deliverable apertures. Furthermore, this aperture is added to the model only if increasing the intensity of that aperture actually corresponds to an *improvement* in the objective function value.

## 3.3. Solving the pricing problem

We will consider the following four common sets of hardware constraints on the set of deliverable apertures:

- (C1) *Consecutiveness constraint* This constraint simply corresponds to the fact that apertures are shaped by pairs of leaves, which means that, in each given bixel row, the exposed bixels should be consecutive.
- (C2) Interdigitation constraint

This constraint says that, in addition to C1, the left leaf of a row cannot overlap with the right leaf of an adjacent row.

(C3) Connectedness constraint This constraint says that, in addition to C2, the bixel rows that contain at least one exposed bixel should be consecutive.

#### (C4) Rectangle constraint

This constraint says that only rectangular apertures may be formed.

Note that constraint C4 corresponds to the use of conventional jaws only. Recently, the viability of this delivery technique has been shown by Kim *et al* (2007) for treating prostate cancer and by Earl *et al* (2007) for treating pancreas, breast and prostate cancer.

Romeijn *et al* (2005) provide polynomial-time algorithms for solving the pricing problem corresponding to C1–C3. In particular, suppose that each beam is discretized into an  $m \times n$  matrix of bixels. They then show that the pricing problem for a particular beam can be solved in O(mn) time for C1 and in  $O(mn^4)$  time for C2 and C3. For completeness sake, we will briefly describe these algorithms below. Next, we will develop an efficient algorithm for solving the pricing problem under C4.

It is easy to see that, under C1, the pricing problem decomposes by a bixel row, i.e., we may find the optimal leaf settings for each row individually and then form the optimal aperture by simply combining these leaf settings. We are thus interested in finding, for each bixel row, a consecutive set of bixels for which the sum of their coefficients in the objective function of the pricing problem is minimal. We can find such a set of bixels by making a single pass, from left to right, through the n bixels in a given row and beam. In doing so, we should keep track of (i) the sum of the coefficients for all bixels considered so far, and (ii) the maximum value of these sums encountered so far. Now note that, at any point in this procedure, the difference between these two is a candidate for the best solution value found so far, so we simply identify the leaf setting that corresponds to the minimum value of this difference. (See also Bates and Constable (1985) and Bentley (1986).)

The algorithm for identifying the optimal aperture to add under C2 and C3 is somewhat more complicated. For these two situations, we formulate the pricing problem as the shortest path problem in an appropriately defined network. In particular, we define a node corresponding to each potential leaf setting in each bixel row, i.e.,  $(r; c_1, c_2)$  for r = 1, ..., mand  $c_1, c_2 = 1, ..., n$  with  $c_1 < c_2$ , where  $c_1$  and  $c_2$  denote the rightmost and leftmost blocked bixel in a row r, respectively. In addition, we define the so-called source and sink nodes representing the 'top' and 'bottom' of the aperture. We then create arcs between nodes that correspond to feasible combinations of leaf settings in the adjacent bixel rows, and assign to any arc leading to a particular node a cost equal to the sum of all coefficients corresponding to the exposed bixels. That is, under C2 we create arcs between a pair of nodes if the interdigitation constraint is satisfied. Under C3, we ignore all nodes that correspond to the bixel rows in which all bixels are blocked; then, in addition to the arcs created for C2, we also create arcs from the source node to all other nodes and from all nodes to the sink node, representing the fact that leaf settings that block all bixels are allowed at the 'top' and 'bottom' of the aperture.

We will next develop a polynomial-time algorithm for the pricing problem associated with C4. For convenience, let (b, r, c) denote the bixel in row r and column c of beam b (r = 1, ..., m; c = 1, ..., n; and  $b \in B$ ). Moreover, let  $(b, r_1, r_2, c_1, c_2)$  represent a rectangular aperture in which  $r_1$  and  $r_2$  denote the first and the last row, while  $c_1$  and  $c_2$  denote the leftmost and rightmost column of bixels which form the rectangular aperture in beam b. We can then formulate the pricing problem for beam b under C4 as follows:

minimize 
$$\sum_{r=r_1}^{r_2} \sum_{c=c_1}^{c_2} \left( \sum_{j \in V} D_{(b,r,c)j} \hat{\pi}_j \right)$$

subject to

$$r_1 < r_2$$
  $c_1 < c_2$   $r_1, r_2 \in \{1, \dots, m\}$   $c_1, c_2 \in \{1, \dots, n\}.$ 

It is easy to see that we can employ the algorithm for C1 to construct an algorithm for C4. In particular, suppose that we fix the range of rows in the rectangular aperture as  $r_1$  and  $r_2$  (with, of course,  $r_1 < r_2$ ). Then the problem reduces to

minimize 
$$\sum_{c=c_1}^{c_2} \left( \sum_{r=r_1}^{r_2} \sum_{j \in V} D_{(b,r,c)j} \hat{\pi}_j \right)$$

subject to

$$c_1 < c_2$$
  $c_1, c_2 \in \{1, \ldots, n\}$ 

which is precisely a pricing problem of the form as for C1 with respect to the *sum* of rows  $r_1, \ldots, r_2$  in the matrix of objective function coefficients. Therefore, *given* these aggregate objective coefficients we can solve the pricing problem for C4 in  $O(m^2n)$  time by enumerating all  $O(m^2)$  possible collections of consecutive rows and selecting the best solution among these candidates. Now note that we can, for each value of  $r_1$ , determine *all* aggregate objective function coefficients in O(mn) time. This means that all objective function coefficients can be determined in  $O(m^2n)$  time, and the running time of the entire algorithm is  $O(m^2n)$ .

Clearly, if, for each beam  $b \in B$ , the best solution found has an objective function value that exceeds the corresponding threshold value (4) derived in section 3.2, no aperture can improve the current solution, which is therefore optimal for (A). Otherwise, adding the optimal aperture, say  $(b^*, r_1^*, r_2^*, c_1^*, c_2^*)$ , to the set  $\hat{K}$  can improve the current solution.

#### 4. Results

#### 4.1. Clinical problem instances

To test our models, three-dimensional treatment planning data for ten head-and-neck cancer patients were exported from a commercial patient imaging and anatomy segmentation system at the University of Florida, Department of Radiation Oncology. These data were then imported into the University of Florida Optimized Radiation Therapy (UFORT) treatment planning system and were used to generate the data required by the models described above.

For all ten cases, we designed plans using five equispaced <sup>60</sup>Co-beams. Note that this does not affect the optimization algorithm, which is, without modification, applicable to high-energy x-ray beams as well (for example, see Romeijn *et al* (2005) for results with 6 MV photon beams). The five beams are evenly distributed around the patient with angles  $0^{\circ}$ ,  $72^{\circ}$ ,  $144^{\circ}$ ,  $216^{\circ}$  and  $288^{\circ}$ , respectively. The nominal size of each beam is  $40 \times 40 \text{ cm}^2$ . The beams are discretized into bixels of size  $1 \times 1 \text{ cm}^2$ , yielding on the order of 1600 bixels. However, we reduce the set of beamlets that actually need to be considered in the optimization by using the fact that the actual volume to be treated is usually significantly smaller. That is, for each beam, we identify a 'mask' consisting of only those bixels that can help treat the targets, i.e., we identify the bixels for which the dose deposition coefficient  $D_{ij}$  associated with at least one target voxel is nonzero. We then extend the mask to a rectangle of minimum size to ensure that all deliverable apertures from C1–C4 that can help treat the targets are considered. For all cases we generated a voxel grid with voxels of size  $4 \times 4 \times 4$  mm<sup>3</sup> for the targets and critical structures, except for unspecified tissue, for which we used voxels of size  $6 \times 6 \times 6$  mm<sup>3</sup>. Table 1 shows the problem dimensions for the ten cases.

Each case contained two targets, which are referred to as planning target volume 1 (PTV1) and planning target volume 2 (PTV2). PTV1 consists of the gross tumor volume (GTV) expanded to account for both sub-clinical disease as well as daily setup errors and internal organ motion; PTV2 is a larger target that also contains high-risk nodal regions, again



**Figure 1.** A typical CT slice illustrating target and critical structure deliniation. In particular, the targets PTV1 and PTV2 are shown, as well as the right parotid gland (RPG), the spinal cord (SC) and normal tissue (Tissue).

Table 1. Model dimensions.

Case	No of structures	No of voxels	No of bixels
1	14	85 017	990
2	13	104 298	1637
3	8	189 234	1658
4	11	195 113	2006
5	12	86 255	1113
6	13	58636	765
7	10	102 262	1247
8	10	84 369	1149
9	10	71837	938
10	12	148 294	2183

expanded to account for sub-clinical disease and setup errors and organ motion. PTV1 and PTV2 have prescription doses of 73.8 Gy and 54 Gy, respectively. Figure 1 shows an example of target deliniation.

Our FMO model employed treatment plan evaluation criteria that are quadratic one-sided voxel-based penalties. In particular, denoting the set of targets by *T* the set of critical structures by *C*, the set of all structures by  $S = T \cup C$ , and the set of voxels in structure  $s \in S$  by  $V_s$ , we use the following treatment plan evaluation criteria:

$$G_{s-}(z) = \frac{1}{|V_s|} \sum_{j \in V_s} (\max\{0, T_s^- - z_j\})^2 \qquad s \in T$$
(5)

$$G_{s+}(z) = \frac{1}{|V_s|} \sum_{j \in V_s} (\max\{0, z_j - T_s^+\})^2 \qquad s \in S.$$
(6)

(Clearly, this means that the set of treatment plan evaluation criteria can be expressed as  $L = \{s - : s \in T\} \cup \{s + : s \in S\}$ .) Criteria (5) penalize underdosing below the underdosing threshold  $T_s^-$  in all targets  $s \in T$ , while criteria (6) penalize overdosing above the overdosing threshold  $T_s^+$  in all structures  $s \in S$ . We choose this model based on the fact that it, in our experience, can be solved very efficiently and yields high-quality treatment plans. However, recall that our algorithm can easily be applied to models that include other convex treatment plan evaluation criteria, such as voxel-based penalty functions with higher powers, or EUD. The resulting model (A) was solved by our in-house primal-dual interior point algorithm (see, Aleman *et al* (2007)). We tuned the problem parameters (underdose and overdose thresholds and criteria weights) by manual adjustment based on two of the ten patient cases and a beamlet-based FMO model. We then used this set of parameters to solve different variants of the beamlet-based and aperture-based FMO problem for all ten patient cases. Finally, all of our experiments were performed on a PC with a 3.4 GHz Intel Pentium IV processor and 2 GB of RAM, running under Windows XP. Our algorithms were implemented in Matlab 7.

# 4.2. Dose-volume histogram (DVH) criteria

Our approach is to employ a convex, and therefore efficiently solvable formulation of the FMO problem. However, we use clinical DVH criteria to objectively verify both the ability of our models to create clinically acceptable treatment plans as well as the robustness of the problem parameters (which, as mentioned above, are not tuned for individual patients). We use the DVH criteria used in the Department of Radiation Oncology at the University of Florida. These criteria are based on the current clinical guidelines formulated by the Radiation Therapy Oncology Group (2000, 2002):

- PTV1
  - At least 99% should receive 93% of the prescribed dose  $(0.93 \times 73.8 \text{ Gy})$ .
  - At least 95% should receive the prescribed dose (73.8 Gy).
  - No more than 10% should be overdosed by more than 10% of the prescribed dose  $(1.1 \times 73.8 \text{ Gy})$ .
  - No more than 1% of PTV1 should be overdosed by more than 20% of the prescribed dose (1.2 × 73.8 Gy).
- PTV2
  - At least 99% should receive 93% of the prescribed dose  $(0.93 \times 54 \text{ Gy})$ .
  - At least 95% should receive the prescribed dose (54 Gy).
- Salivary glands (right and left parotid glands, right and left submandibular glands).
  - No more than 50% of each gland should receive more than 30 Gy.
- Other structures.
  - Tissue should receive less than 60 Gy.
  - Spinal cord should receive less than 45 Gy.
  - Mandible should receive less than 70 Gy.
  - Brain stem should receive less than 54 Gy.
  - Eye should receive less than 45 Gy.
  - Optic nerve should receive less than 50 Gy.
  - Optic chiasm should receive less than 55 Gy.

#### 4.3. Stopping rules

We use the column generation algorithm to solve the aperture-based FMO problem. In our implementation, we identify in each iteration the best aperture (among all beams) that could improve the treatment plan quality, and add this aperture to the set of apertures currently under consideration. This approach allows us to make a trade-off between the number of apertures and the treatment plan quality. As the number of apertures increases, at some point the improvement in treatment plan quality may no longer be clinically significant. Moreover, a high number of apertures in general leads to a high beam-on time. Hence, rather than allowing the column generation algorithm to formally converge, we propose to terminate the algorithm based on the observed development of the clinical DVH criteria. In particular, we investigate the merits of the following two stopping rules:

• Convergence:

This stopping rule is based on observing that treatment plan quality, with respect to a particular criterion, has not improved markedly in recent iterations. More formally, we say that we are satisfied with the solution with respect to a particular criterion if, in the last five iterations, the range of observed criterion values spans less than  $\delta$  (where we use  $\delta = 0.5\%$  for target criteria and  $\delta = 2\%$  for critical structure criteria).

• Clinical:

This stopping rule is based on observing that the treatment plan performance with respect to a clinical criterion has been satisfactory in the last five iterations. More formally, we say that we are satisfied with the solution with respect to a particular criterion if *either* the first stopping rule is satisfied *or*, in the last five iterations, the clinical DVH criterion is satisfied, allowing for a 1% error bar in all but one of those iterations. (Note that we allow for the clinical stopping rule to be 'satisfied' if the convergence stopping rule is satisfied to account for the fact that certain clinical criteria cannot be achieved. This may, for example, be the case if a critical structure is wholly or partially contained in a target.)

In either case, we say that the algorithm has converged if the stopping rule has been satisfied for all convergence (respectively clinical) criteria. Moreover, we report the solution obtained in the first iteration of the last sequence of five iterations.

# 4.4. Results

We divide the discussion of our results into two parts according to the goals that we formulated in section 1. First, we evaluate the ability of our approach to efficiently find high-quality treatment plans with a limited number of apertures, as well as the effect of MLC deliverability constraints on the required number of apertures and beam-on time. Next, we evaluate the importance of explicitly incorporating transmission effects into the optimization model. However, before we do so, in figures 2 and 3 we illustrate the behavior of our FMO model by showing the DVHs and isodose curves superimposed on a typical CT slice, both corresponding to an optimal treatment plan found for case 5. The isodose curves show both the conformality of the plan with respect to the two targets and the sparing of the spinal cord and saliva glands.

4.4.1. Delivery efficiency. Tables 2 and 3 show the number of apertures and beam-on time (in minutes) for the ten cases obtained with our aperture-based approach. We used the two stopping rules described in section 4.3. For these experiments, we have not incorporated any transmission effects. For comparison purposes, the tables also show the results of traditional beamlet-based FMO where the optimal fluence maps were first discretized to integer multiples of 5% of the maximum beamlet intensity in each beam, and subsequently decomposed into



Figure 2. DVHs of the optimal treatment plan obtained for case 5 with C1 aperture constraints and the convergence stopping rule.



**Figure 3.** Isodose curves for 73.8 Gy, 54 Gy and 30 Gy on a typical CT slice, corresponding to the optimal treatment plan obtained for case 5 with C1 aperture constraints and the convergence stopping rule.

apertures with the objective function of minimizing the beam-on time. We used the algorithms by Kamath *et al* (2003, 2004a) to minimize the beam-on time under C1 and C2, respectively. Furthermore, we applied a modification of the approach by Boland *et al* (2004) to minimize the

Direct aperture optimization in IMRT treatment planning

		Table 2	. Numbe	er of aper	tures wit	hout trans	smission	effects.				
				Apertu	ire-based	1						
		Cli	nical			Conve	rgence			Beamle	et-based	
Case	C1	C2	C3	C4	C1	C2	C3	C4	C1	C2	C3	C4
1	17	29	22	59	57	48	51	142	170	189	329	334
2	35	45	33	115	47	47	33	132	213	230	390	650
3	19	19	20	33	35	31	33	39	212	252	384	592
4	23	24	24	51	29	29	24	52	262	293	449	636
5	32	19	26	42	39	37	64	55	185	227	348	378
6	18	29	42	52	54	65	93	83	183	211	285	321
7	18	18	19	32	49	22	30	55	196	219	357	445
8	50	72	86	137	77	100	86	137	173	198	327	394
9	19	20	23	38	30	30	27	66	181	203	312	384
10	17	19	19	47	24	27	34	59	248	295	418	611
Average	24.8	29.4	31.4	60.6	44.1	43.6	47.5	82.0	202.3	231.7	359.9	474.5

Table 3. Beam-on time without transmission effects.

				Apertui	re-based							
		Cli	nical			Conv	ergence			Beamle	et-based	
Case	C1	C2	C3	C4	C1	C2	C3	C4	C1	C2	C3	C4
1	2.56	2.90	2.70	6.59	3.98	3.52	3.56	12.43	7.43	8.23	14.51	14.67
2	2.98	3.09	2.77	9.14	3.21	3.12	2.77	9.84	8.46	9.16	15.65	26.00
3	2.92	2.72	2.70	4.66	3.30	3.08	3.06	4.98	8.07	9.43	14.48	22.86
4	2.73	2.68	2.65	6.26	2.89	2.82	2.65	6.30	10.35	11.68	18.85	27.19
5	3.24	2.60	2.78	5.05	3.49	3.09	3.89	6.13	8.94	10.95	17.52	19.45
6	2.56	2.72	3.26	5.00	3.54	3.69	4.06	6.91	6.81	7.81	10.70	12.11
7	2.56	2.52	2.49	3.98	3.30	2.62	2.82	5.77	7.98	8.79	14.11	18.00
8	4.04	4.42	4.68	12.12	4.48	4.92	4.68	12.12	7.31	8.35	13.92	16.81
9	2.65	2.56	2.69	4.42	3.12	2.96	2.82	6.29	7.09	7.70	12.51	17.18
10	2.72	2.76	2.70	6.86	2.97	2.97	3.25	7.99	10.71	12.81	18.33	26.79
Average	2.89	2.89	2.94	6.41	3.42	3.28	3.36	7.87	8.31	9.50	15.05	20.10

beam-on time under C3, while we used a linear programming model for the case of C4. (Note that there are, in general, many decompositions that attain the minimum beam-on time; the number of apertures that is given is for a particular solution that the so-called leaf-sequencing algorithm found, but that number is not minimized explicitly.)

Our main conclusions are given as follows:

- With our direct aperture optimization approach and based on our stopping rules, we conclude that the number of apertures required under aperture constraints C1-C3 is, on average, on the order of 30-45, increasing to 60-85 with jaws-only delivery.
- The direct aperture optimization approach leads to a reduction of the required number of apertures by, on average, more than 75% of the number obtained with the traditional two-phase approach. Moreover, the required beam-on time is reduced by, on average, more than 50%.
- There is very little effect on the required number of apertures and beam-on time when interdigitation or connectedness constraints are imposed; however, the required number of apertures and beam-on time increase by, on average, approximately 50% when only rectangular apertures are considered.



Figure 4. Case 5: the relative volume of (a) PTV1 and (b) PTV2 that receives in excess of its prescription dose.

It is interesting to see that in some cases fewer apertures are required when the deliverability constraints are strengthened. This is caused by a combination of the fact that our approach does not explicitly minimize the number of apertures and the fact that the effect of some constraints (in particular, the added constraint in C3 as compared to C2) is apparently negligible in practice.

The amount of time required, on average, by our optimization algorithm to find the aperture-based solutions ranges from about 1–3 min of the CPU time for the case of consecutiveness constraints only. The required time increases up to 4 min when interdigitation and connectedness are imposed, while it further increases up to about 12 min when only rectangular apertures are allowed. This is in comparison with an average of a little over 1 min of the CPU time required for the traditional two-phase approach. Note that these times do not include the time required to read the DICOM data and compute the dose deposition constraints, which took about 10–25 min of the CPU time depending on the size of the case. However, note that these tasks only need to be performed once for each patient.

To illustrate how our approach may be used to make a trade-off between treatment plan quality and delivery efficiency, figures 4 and 5 show the behavior of target coverage and



Figure 5. The relative volume of (a) LSG and (b) RSG that receives in excess of 30 Gy.

submandibular gland sparing as a function of the number of apertures used for C1–C4 for a typical example, case 5.

4.4.2. Transmission effects. We have also studied the effect of incorporating transmission effects into the FMO problem. First, tables 4 and 5 show the number of apertures and beam-on time with incorporation of transmission effects. We have used  $\epsilon = 1.7\%$  as the transmission rate (see, Arnfield *et al* (2000)). A comparison with tables 2 and 3 reveals that the incorporation of transmission effects has very little effect on the treatment delivery efficiency.

Next, tables 6–8 show the results of the aperture-based FMO problem under C1 without and with transmission effects using the convergence stopping rule. In particular, the tables show values of the DVH criteria for the targets and main critical structures for all ten cases. For example, the data in the column labeled PTV2@93% represents the fraction of volume (in %) of PTV2 receiving  $0.93 \times 54$  Gy. The labels of the other columns follow a similar format, where the acronyms correspond to the left parotid gland (LPG), right parotid gland (RPG), left submandibular gland (LSG) and right submandibular gland (RSG). Comparing tables 6 and 8 suggests that treatment plans of very similar quality can be found with and without incorporation of transmission effects. However, the results of table 6 neither incorporate transmission in the optimization problem nor account for transmission in the presentation of

		Cli	nical			Conve	rgence	
Case	C1	C2	C3	C4	C1	C2	C3	C4
1	26	25	29	87	44	32	102	106
2	32	31	38	79	35	62	59	140
3	17	18	16	36	37	23	23	51
4	28	32	20	39	28	32	29	63
5	23	24	24	68	60	68	31	68
6	24	31	27	49	79	76	43	55
7	24	17	22	24	41	41	30	68
8	68	74	66	138	70	74	66	138
9	18	19	20	23	56	68	55	81
10	16	21	22	33	27	36	34	51
Average	27.6	29.2	28.4	57.6	47.7	51.2	47.2	82.

Table 4. Aperture-based FMO: number of apertures with transmission effects.

 Table 5. Aperture-based FMO: beam-on time with transmission effects.

		Clir	nical			Conver	gence	
Case	C1	C2	C3	C4	C1	C2	C3	C4
1	2.84	2.80	2.89	7.17	3.44	2.97	4.04	7.65
2	2.84	2.68	2.78	6.62	2.92	3.25	3.18	8.91
3	2.70	2.65	2.58	4.70	3.24	2.74	2.76	5.55
4	2.78	2.81	2.53	5.05	2.78	2.81	2.72	6.10
5	2.72	2.64	2.65	6.83	3.69	3.81	2.96	6.83
6	2.65	2.82	2.60	4.65	3.69	3.65	2.94	4.70
7	2.65	2.46	2.53	3.42	3.08	3.02	2.72	5.25
8	4.04	4.09	3.78	8.23	4.06	4.09	3.78	8.23
9	2.56	2.50	2.52	3.36	3.68	3.76	3.56	6.47
10	2.61	2.78	2.90	4.85	2.96	3.22	3.16	6.11
Average	2.84	2.82	2.78	5.49	3.36	3.33	3.18	6.58

Table 6. Aperture-based FMO: DVH criteria under C1 without transmission effects.

	PTV2	PTV2	PTV1	PTV1	PTV1	PTV1	LPG	RPG	LSG	RSG
Case	@ 93%	@ 100%	@ 93%	@ 100%	@ 110%	@ 120%	@ 30 Gy	@ 30 Gy	@ 30 Gy	@ 30 Gy
1	99.4	98.7	100.0	99.0	4.5	0.0	21.8	18.5	33.1	100.0
2	99.1	98.9	99.7	97.9	9.9	0.0	49.3	100.0	100.0	100.0
3	99.8	99.6	100.0	99.3	2.7	0.0	20.4	18.3	n/a	n/a
4	98.8	98.0	100.0	100.0	2.7	0.0	10.3	4.1	54.1	17.7
5	98.6	97.7	100.0	100.0	8.1	0.0	42.2	0.0	44.4	34.6
6	99.5	99.0	100.0	98.6	6.7	0.0	26.2	36.2	n/a	n/a
7	99.1	98.6	100.0	99.2	2.4	0.0	0.5	46.7	24.6	100.0
8	99.2	98.9	100.0	98.6	9.9	0.0	28.6	4.9	100.0	52.3
9	99.2	98.1	100.0	99.6	2.1	0.0	5.9	39.8	36.4	100.0
10	100.0	100.0	100.0	100.0	4.3	0.0	0.2	25.4	7.7	100.0

the actual results, so that the treatment plan quality in that table is a *perceived* rather than an actual one. Table 7 shows the actual quality of the treatment plan that was obtained when

Direct aperture optimization in IMRT treatment planning

		<b>Table 7</b> optimiza	• Apertur ation.	e-based FN	MO: DVH	criteria und	ler C1 with	transmissio	on effects a	dded after
Case	PTV2 @ 93%	PTV2 @ 100%	PTV1 @ 93%	PTV1 @ 100%	PTV1 @ 110%	PTV1 @ 120%	LPG @ 30 Gy	RPG @ 30 Gy	LSG @ 30 Gy	RSG @ 30 Gy
1	99.6	99.2	100.0	99.9	19.5	0.0	23.8	21.4	38.6	100.0
2	99.3	99.0	99.9	99.0	34.0	0.0	51.0	100.0	100.0	100.0
3	99.8	99.7	100.0	100.0	24.3	0.0	21.8	19.1	n/a	n/a
4	98.8	98.1	100.0	100.0	20.9	0.0	10.5	4.1	55.7	17.7
5	98.8	98.1	100.0	100.0	30.6	0.0	43.0	0.0	46.8	39.5
6	99.6	99.2	100.0	99.2	25.7	0.0	28.2	38.4	n/	n/a
7	99.2	98.8	100.0	99.8	15.0	0.0	0.7	48.2	29.8	100.0
8	99.3	99.0	100.0	100.0	41.6	0.0	29.5	5.5	100.0	58.1
9	99.5	98.8	100.0	99.9	18.9	0.0	7.2	46.1	40.2	100.0
10	100.0	100.0	100.0	100.0	11.2	0.0	0.2	25.4	9.1	100.0

Table 8. Aperture-based FMO: DVH criteria under C1 with transmission effects.

Case	PTV2 @ 93%	PTV2 @ 100%	PTV1 @ 93%	PTV1 @ 100%	PTV1 @ 110%	PTV1 @ 120%	LPG @ 30 Gy	RPG @ 30 Gy	LSG @ 30 Gy	RSG @ 30 Gy
1	99.3	98.4	99.7	96.9	4.9	0.0	22.9	20.2	33.1	100.0
2	99.0	98.6	99.9	97.5	6.7	0.0	44.6	100.0	100.0	100.0
3	99.7	99.6	100.0	99.3	1.3	0.0	20.0	18.1	n/a	n/a
4	98.4	97.5	100.0	100.0	2.4	0.0	9.5	1.4	53.0	15.6
5	98.5	97.7	100.0	99.4	3.1	0.0	38.9	0.0	42.7	33.3
6	99.3	98.9	100.0	97.4	4.0	0.0	24.8	35.7	n/a	n/a
7	99.0	98.4	100.0	99.1	0.5	0.0	0.5	47.5	17.5	100.0
8	98.9	98.6	100.0	97.7	8.8	0.0	26.9	3.9	100.0	48.9
9	99.1	98.3	100.0	99.2	1.2	0.0	2.6	35.1	33.6	100.0
10	100.0	100.0	100.0	100.0	8.6	0.0	0.2	23.1	1.4	100.0

Table 9. Beamlet-based FMO: DVH criteria under C1 without transmission effects.

_	PTV2	PTV2	PTV1	PTV1	PTV1	PTV1	LPG	RPG	LSG	RSG
Case	@ 93%	@ 100%	@ 93%	@ 100%	@ 110%	@ 120%	@ 30 Gy	@ 30 Gy	@ 30 Gy	@ 30 Gy
1	99.4	99.0	99.9	98.3	5.0	0.0	19.4	17.5	32.3	100.0
2	99.2	98.8	99.9	98.7	3.8	0.0	43.0	96.7	100.0	100.0
3	99.8	99.7	100.0	99.7	2.6	0.0	19.3	17.8	n/a	n/a
4	98.8	98.3	100.0	100.0	1.1	0.0	9.0	1.6	53.0	16.7
5	98.8	98.1	100.0	100.0	3.1	0.0	37.7	0.0	39.5	32.1
6	99.9	98.9	100.0	98.3	8.4	0.0	24.2	34.3	n/a	n/a
7	99.2	98.8	100.0	99.1	1.8	0.0	0.3	46.5	14.9	100.0
8	99.2	98.9	100.0	99.3	14.1	0.0	28.3	4.4	100.0	51.7
9	99.3	98.6	100.0	98.6	0.5	0.0	2.1	34.6	33.6	100.0
10	100.0	100.0	100.0	100.0	3.7	0.0	0.2	22.8	0.0	100.0

solving an optimization model that does not take transmission effects into account, i.e., for the results in table 7 transmission effects were added *a posteriori* to the plan.

Finally, we analyzed the results of using a beamlet-based FMO approach followed by a leaf-sequencing phase, under C1. Table 9 shows the perceived quality of the obtained treatment plan (in which transmission effects are ignored), while table 10 shows the actual

C Men et al

		Table 10	). Beamle	t-based FM	O: DVH cr	iteria under	C1 with tra	nsmission e	effects.	
Case	PTV2 @ 93%	PTV2 @ 100%	PTV1 @ 93%	PTV1 @ 100%	PTV1 @ 110%	PTV1 @ 120%	LPG @ 30 Gy	RPG @ 30 Gy	LSG @ 30 Gy	RSG @ 30 Gy
1	99.9	99.8	100.0	100.0	69.1	1.3	32.5	27.2	55.1	100.0
2	99.6	99.5	100.0	99.9	96.5	0.4	59.1	99.3	100.0	100.0
3	99.9	99.9	100.0	100.0	94.3	0.1	25.8	21.0	n/a	n/a
4	99.7	99.5	100.0	100.0	100.0	6.8	17.7	10.4	74.6	40.3
5	99.6	99.3	100.0	100.0	83.1	1.3	48.0	2.1	56.5	56.8
6	99.9	99.4	100.0	100.0	75.8	0.0	33.6	41.7	n/a	n/a
7	99.7	99.5	100.0	100.0	96.7	1.8	4.4	59.3	42.1	100.0
8	99.7	99.5	100.0	100.0	86.9	1.4	40.2	18.5	100.0	70.69
9	99.8	99.7	100.0	100.0	72.7	0.0	9.4	54.5	51.4	100.0
10	100.0	100.0	100.0	100.0	100.0	70.6	4.7	41.7	16.1	100.0

quality of the treatment plan (in which transmission effects are added to the final treatment plan).

From the latter two tables, it is clear that using a beamlet-based FMO optimization approach may severely underestimate target hotspots (overdosing) and effects on critical structures. The direct aperture optimization approach with transmission effects incorporated, however, provides a high-quality treatment plan with, on average, a comparable number of apertures and beam-on time. Taking case 5 as an example, a treatment plan that ignored transmission effects appeared to spare all four saliva glands, while less than 10% of PTV1 received in excess of 110% of its the prescription dose. Adding transmission effects to the plan found using beamlet-based FMO showed that in fact only two saliva glands were spared with the PTV1 hotspot increasing to over 80%. Incorporating transmission effects into the aperture-based FMO model showed that it was possible to spare all saliva glands and that keep the dose to PTV1 in excess of 110% of its prescribed dose to about 3%.

### 5. Concluding remarks and future research

In this paper, we used a direct aperture optimization approach to design radiation therapy treatment plans for individual patients. This approach allows us to make a sound trade-off between treatment plan quality and delivery efficiency. In addition, our model is able to explicitly incorporate transmission effects, which can dramatically affect the quality of a treatment plan but are ignored by the most existing FMO models. Future research could extend the research in this paper by explicitly incorporating a measure of treatment plan efficiency, such as beam-on time, into the optimization model.

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